

Spring undeformed when inclination  $\alpha$ , ( $P=0$ )  
 Displacement  $\theta$  as shown from undeformed state.

Set  $\phi = \alpha - \theta$  ;  $\phi' = -1$  ;  $' \equiv d/d\theta$ .

Load displacement =  $\frac{P}{2} (\sin \alpha - \sin \phi)$ .

Spring deflexion =  $l (\cos \phi - \cos \alpha)$

$\therefore$  Energy =  $\frac{1}{2} k l^2 (\cos \phi - \cos \alpha)^2 + P \frac{1}{2} l (\sin \phi - \sin \alpha)$

Set  $V = \text{energy} / k l^2$  ; &  $p = P / 2 k l$   
 $= \frac{1}{2} (\cos \phi - \cos \alpha)^2 + p (\sin \phi - \sin \alpha)$

$\therefore V' = (\cos \phi - \cos \alpha) \sin \phi - p \cos \phi$

$V'' = -\cos 2\phi + \cos \alpha \cos \phi - p \sin \phi$

For equilibrium,  $V' = 0$ , so

①  $p = (1 - \cos \alpha / \cos \phi) \sin \phi$  ;  $\phi = \alpha - \theta$

$V'' = (\cos \alpha - \cos^3 \phi) / \cos \phi$

- from which it may be deduced that if  $\cos^3 \phi > \cos \alpha$   
 i.e. if  $9.4^\circ < \theta < 35.6^\circ$  (with  $\alpha = 22.5^\circ$ ),  $V'' < 0$   
 and the structure is unstable. If  $\theta < 9.4^\circ$  or  
 $\theta > 35.6^\circ$  the structure is stable.

Neutral equilibrium occurs when  $\theta = 9.4^\circ$  or  $35.6^\circ$   
 i.e. when  $\cos \phi = (\cos \alpha)^{1/3}$ , or, when

$\cos \theta = \cos^{1/3} \alpha \pm \sin \alpha (1 - \cos^{2/3} \alpha)^{1/2}$

corresponding to local minima/maxima given by ① as:

$\delta = \pm (1 - \cos^{2/3} \alpha)^{3/2} = \pm 0.0117$

The above characteristics are confirmed by the plot of  
 ① vs.  $\theta$ , shown overleaf for  $\alpha = 22.5^\circ$ .

Consider what happens to the structure as both the  
 displacement  $\theta$  and the load  $p$  ( $P$ ) increase from zero  
 under two different physical constraints: -

Displacement controlled.

Here the loading device is arranged to increase  
 $\theta$  monotonically and to supply the necessary force,  
 as dictated by the structure's characteristic, automatically.  
 Hence the full-line characteristic is traced out.

Load controlled.

In this arrangement, which is the simplest and  
 most common, the loading device increases the force  
 monotonically, the structure being allowed to  
 assume whatever geometry (displacement) it wishes.  
 As this load is increased from zero to the point A,  
 an infinitesimal increase causes the dashed  
 trajectory A-B to be undergone, with consequent  
 instantaneous increase in displacement. This  
 highly non-linear instability (temporary) is known  
 as SNAP. Further increase of load beyond B is  
 uneventful.

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